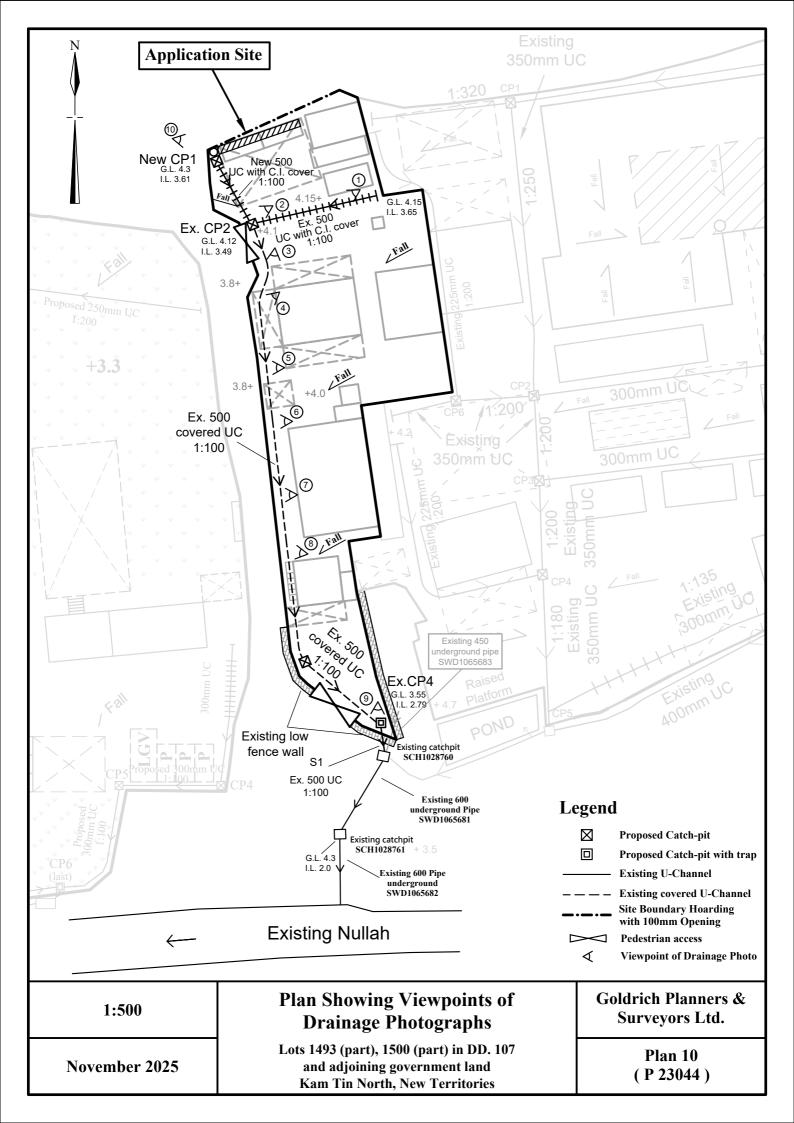


| 1 For Catchment Area of Subject Site | | | | | Ref. |
|---|------------------|--|---|-----------|------------------------------------|
| Δrea | Δ = | 1381 | m^2 | | |
| Average slope, | H = | 0.1 | m per 100m | | |
| Distance on the line of natural flow, | L = | 25 | | | |
| Time of concentraction, | t _o = | , | , , , , | 1381^0.1) | SDM 7.5.2 (d) |
| = 2.8 min 2 For Existing 500mm U-Channel to SCH1028760 | | | | | |
| | From | То | | | |
| Ground level (mPD) | 4.30 | 3.55 | • | | |
| Invert level (mPD) | 3.61 | 2.75 | | | |
| Width of u-channel, | \A/ - | 500 | mm | | |
| Length of u-channel, | | | | | |
| Depth of vertical part of u-channel, | | | mm | | |
| Gradient of u-channel, | | | | | |
| Gradient of d-charmer, | o _f – | (3.01-2.73)/60 | - 0.0100 | | |
| Cross-Section Area, | a = | $0.5 \pi r^2 + w d$ | = 0.5 x 3.14 x 250^2 + 500 x 550 | 0 x 0.9 | SDM 9.3 (b) |
| | = | 0.336 | m^2 | | Sedimentation Reduction |
| Wetted Perimeter, | p = | $\pi r + 2 d$ | m ² = 3.14 x 250 + 2 x 550 | | |
| | = | 1.885 | m | | |
| Hydralic radius, | R = | a/p | | | SDM 8.2.1 |
| | = | 0.178 | m | | |
| 2 Use Manning Equation for or | stima | ting valoaity of a | tormustor | | |
| 3 Use Manning Equation for estimating velocity of stormwater | | | | | |
| Take | n = | 0.016 | for concrete lined channels:- | | SDM Table 13 |
| Allowable velocity. | v = | $R^{1/6}x (RS_f)^{1/2}/n$ | $= (0.178)^1/6 \times (0.178 \times 0.01)^1/$ | 2 / 0.016 | SDM Table 12 |
| , | = | | | | |
| Time of flow, | t _f = | | min | | |
| 4 Use "Rational Method" for calculation of design flow | | | | | |
| Design intensity, | | o / /+ + + +b) ^c | | | SDM 4.3.2 |
| Design intensity, | | · · | 29)^0.355 for return period T = 50 y | /oare | |
| | _ | ` | 29) 0.35; for return period 1 = 50 y | /ears | Corrigendum 1/2024 SDM Table 3a |
| | _ | 250 | | | ODIVI TABLE SA |
| Type of surface | | Runoff Coefficient C | Catchment Area A (m ²) | CxA | SDM 7.5.2 (b) |
| Flat Glassland(heavy soil) | | 0.25 | 0.0 | 0.0 | 0DIII 1.0.2 (D) |
| Concrete Paving | | 0.95 | 1381.0 | 1312.0 | |
| | | | SUM = | 1312.0 | |
| | | | | | |
| Upstream flow, | $Q_u =$ | 0 | m ³ /s | | |
| | _ | | | | |
| Design flow, | | | S + Q _u where A _j is in km ² | | SDM 7.5.2 (a) |
| | = | | .95 / 1000000 x 1.16 + 0 | | Corrigendum 1/2022 |
| | = | 0.108 | m ³ /s | | |
| | _ | | | | |
| Allowable flow, | | | | | |
| | | 0.336 x 1.98 | 3. | | |
| | = | 0.598 | mˇ/s | | |
| > 0.(0K) | | | | | |
| > Q _d (O.K.) | | | | | |
| Reference was made to Stormwater Drainage Manual (SDM) by DSD | | | | | |
| | | Плудмать | ia Calculation | Goldrich | n Planners & |
| Scale: NA | | Hyuraul | ic Calculation | | eyors Ltd. |
| | | Lots 1486 | 5 (Part), 1489 (Part) | | • |
| November 2025 | | and adjoining Government Land in D. D. 107 | | | age 1 |
| | | | en Long, N. T. | (P: | 23044) |
| | | | | | |



Your Ref.: A/YL-KTN/1177
Our Ref.: P23044

Viewpoint 1





Your Ref.: A/YL-KTN/1177
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Viewpoint 3





Your Ref.: A/YL-KTN/1177 Our Ref.: P23044



Viewpoint 6





Viewpoint 8



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Viewpoint 9



Viewpoint 10



The ground level of the Site has been higher than the local track for many years. The surface runoff from the local track will not flow to the Site.